

**Ultra-low noise and low-temperature readout electronics $f < 1\text{GHz}$
based on cryoHEMTs made at C2N (formerly LPN):
performance and applications**

Y. Jin, Q. Dong, L. Couraud, A. Cavanna, U. Gennser, C. Ulysse, E. Cambril

C2N, CNRS, Univ. Paris-sud, Univ. Paris-Saclay, Marcoussis, France

moving to:

C2N, CNRS, Univ. Paris-sud, Univ. Paris-Saclay, Palaiseau, France

Outline

- Introduction
 - Motivation
 - Low temperature and low noise *vs* FETs
 - From HEMT to cryoHEMT
- Performance
 - Noise voltage: $\text{sub-nV}/\sqrt{\text{Hz}}$
 - Noise current: $\text{aA}/\sqrt{\text{Hz}}$
- Applications
- Conclusions and further developments

Why low-temperature electronics and the challenge 1/2

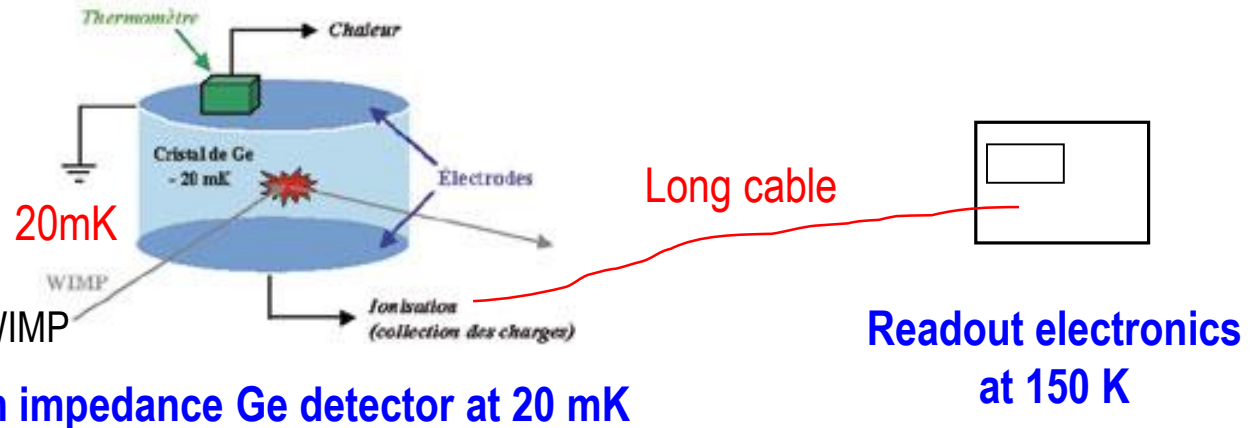
- For most ultra-sensitive detectors: low-temperature → low thermal noise
- $(4kTR)^{1/2} \rightarrow 50M\Omega$: at 300K \Leftrightarrow 910nV/Hz^{1/2}; at 30mK \Leftrightarrow 9.1nV/Hz^{1/2}



CDMS

Cryogenic Dark Matter Search

weakly interacting massive particle: WIMP



High impedance Ge detector at 20 mK

due to the long cable:

- High capacitance → slow down the data acquisition rate
 - Microphonic noise
 - Triboelectricity
 - Capacitive coupling
- } degrade the intrinsic detectors' performance

➔ High performance electronics for high-impedance cryogenic readout electronics

Low temperature, low power and low-frequency noise

Why low-temperature electronics and the challenge 2/2

Present Low Noise Electronics & Operating Conditions

	Low Frequency		High Frequency	
	Low Impedance	High Impedance	Low Impedance	
Room Temperature	HEMTs BJTs	JFETs	HEMTs	commercially available devices
Low Temperature ($T < 100$ K)	HEMTs $f \geq$ MHz	?	HEMTs $f > 1$ GHz	commercially available devices

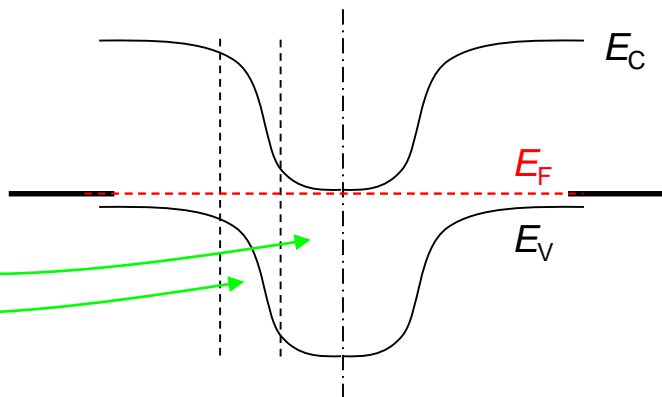
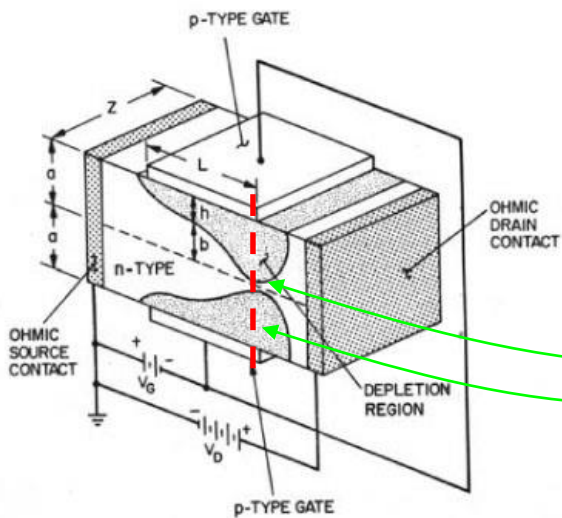
➔ **The challenge is to fill the above gap:**

High performance electronics for high-impedance cryogenic readout electronics

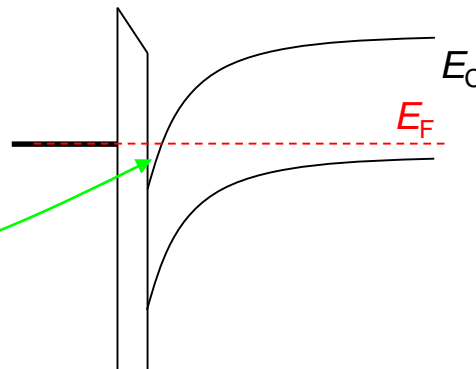
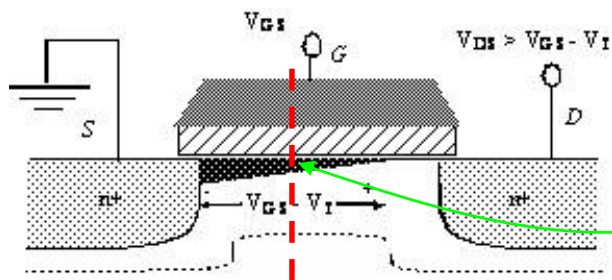
Low temperature, low power and low-frequency noise

Low temperature (LT) and low-frequency (LF) noise vs FETs

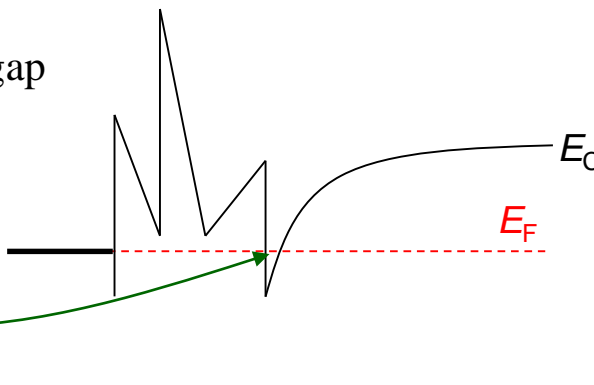
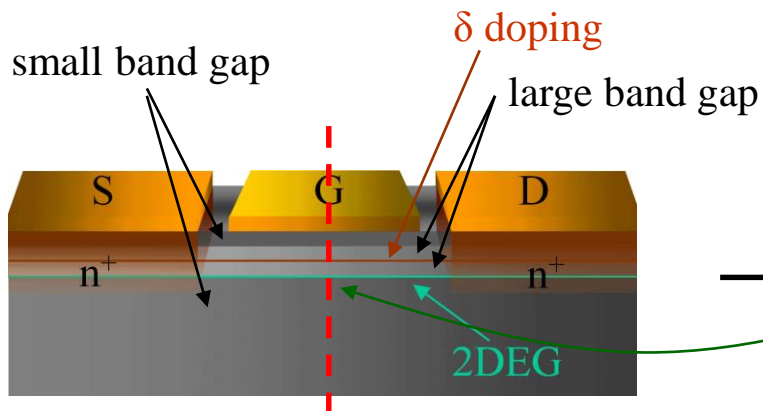
- comparison JFET, MOSFET and HEMT



non degenerate e-
freeze-out at LT
limit: $T > 100K$
gate // P-N
low $1/f$ noise



degenerate e-
no LT limit
gate // oxide layer
high $1/f$ noise

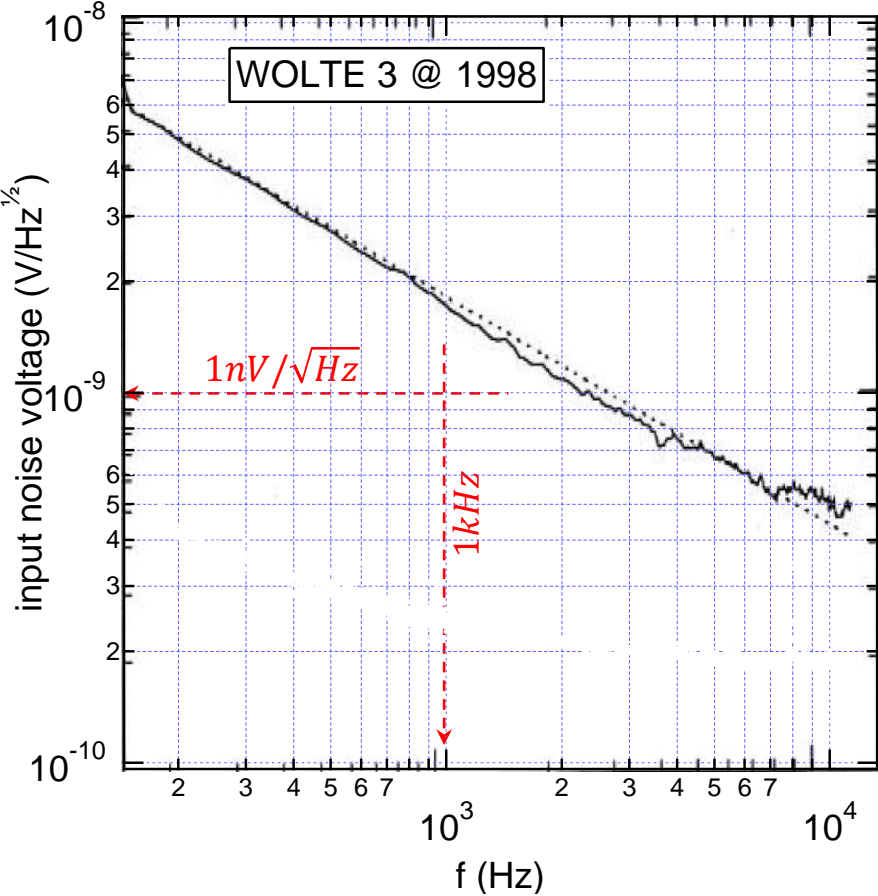


degenerate e-
no LT limit
gate // large bandgap
 $1/f$ noise ?

From HEMT to cryoHEMT

During a long period:

the input noise voltage $> 1 \text{ nV}/\sqrt{\text{Hz}}$ @ 1kHz and 4.2 K



From HEMT to cryoHEMT

More than 10 years collective efforts for optimizing:

Heterostructures by Molecular Beam Epitaxy:

A. Cavanna; U. Gennser

several tens of heterostructures tested

Ohmic and Schottky contacts:

L. Couraud, L. Leroy, A. Durnez, C. Ulysse

EBL (Electron Beam Lithography) and IBE (Ion Beam Etching):

E. Cambril, S. Guilet

several thousands of HEMTs with 4 to 6 steps of EBL

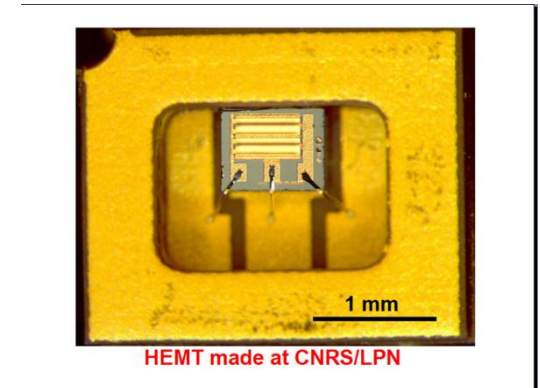
Characterization and simulation:

Q. Dong (PhD & Postdoc since 2009),

YX. Liang (Postdoc 2007-2012), E. Grémion (PhD 2005-2008),

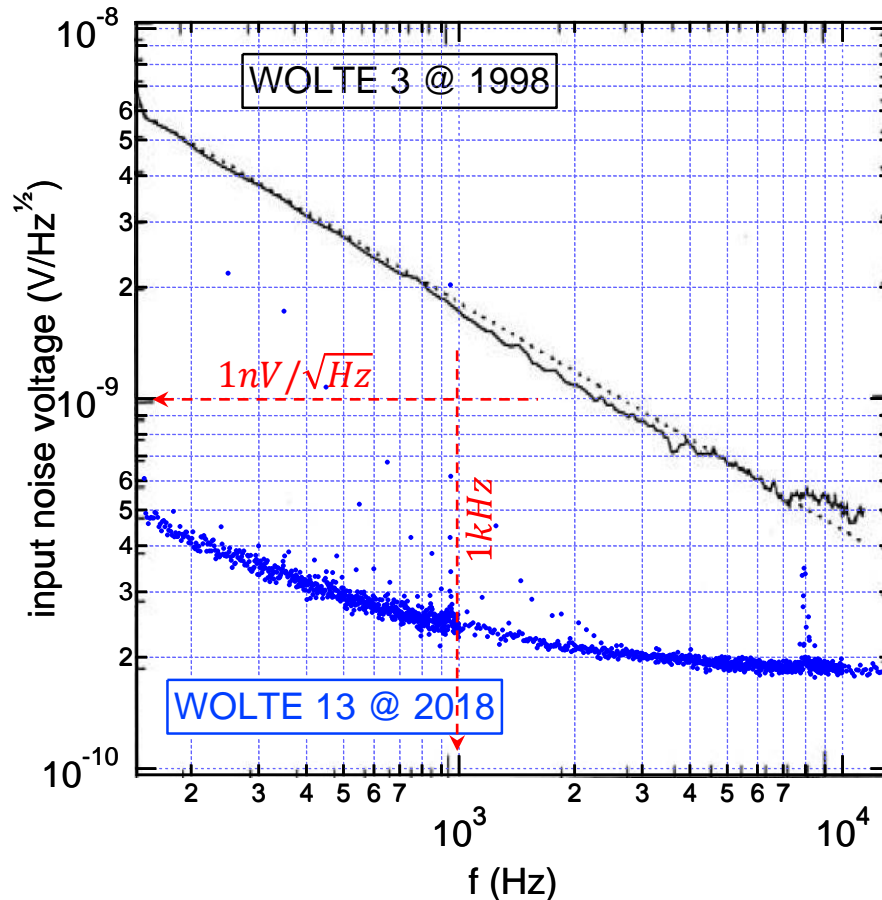
M.C. Cheng, Clarkson Univ. NY (visiting scientist 2007)

several hundreds transistors measured from 300 K to 4.2 K



From HEMT to cryoHEMT

The breakthrough was achieved in 2012 and since then:
the input noise voltage can be $\ll 1 \text{ nV}/\sqrt{\text{Hz}}$ @ 1kHz and 4.2 K



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Characterization: Noise voltage & noise current

Directly measurable parameters:

Channel voltage PSD

$$S_{v-drain} \quad (\text{Power Spectral Density})$$

Voltage gain

$$A_v = \delta V_{out(ds)} / \delta V_{in(gs)}$$

Deduced parameters:

Equivalent input voltage PSD

$$e_{nt}^2 = S_{v-drain} / A_v^2$$

Total equivalent input noise voltage

$$e_{nt} = \sqrt{e_n^2 + e_{ni}^2}$$

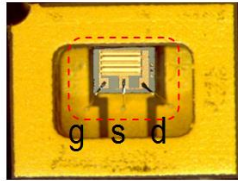
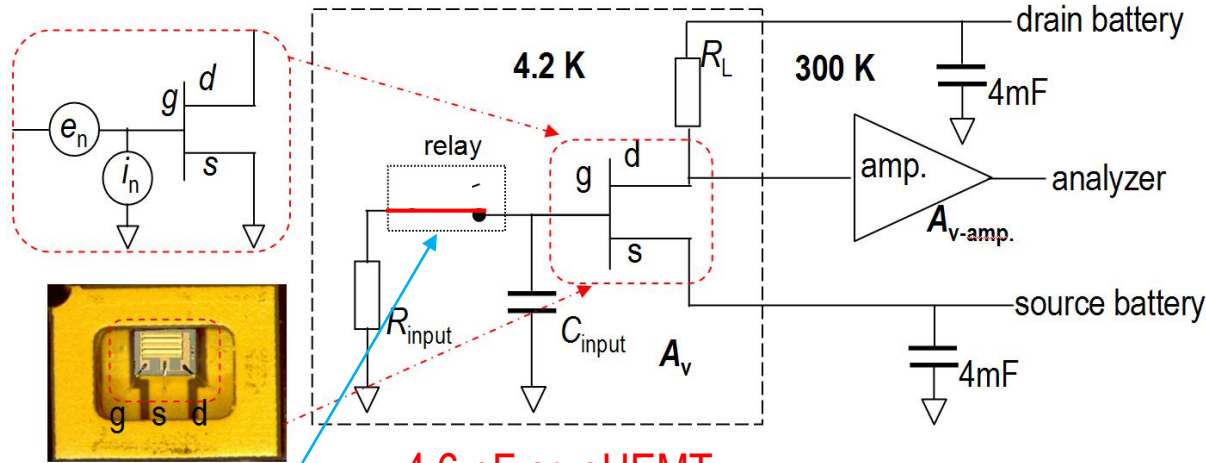
Input noise voltage (with R input)

when $e_{ni} \ll e_n$

$$e_n = e_{nt}$$

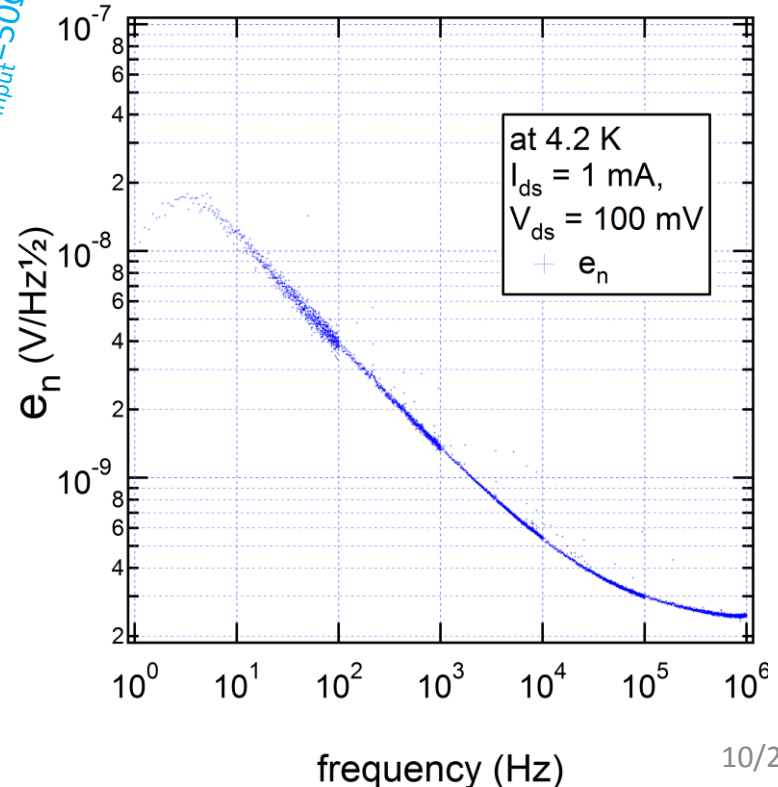
Input noise current (with R & C input)

$$i_n = \sqrt{e_{nt}^2 - e_n^2} / |z| = e_{ni} / |z|$$



4.6 pF cryoHEMT

Noise voltage measurement setup with $R_{input} = 50\Omega$



Characterization: Noise voltage & noise current

Directly measurable parameters:

Channel voltage PSD

$$S_{v-drain} \quad (\text{Power Spectral Density})$$

Voltage gain

$$A_v = \delta V_{out(ds)} / \delta V_{in(gs)}$$

Deduced parameters:

Equivalent input voltage PSD

$$e_{nt}^2 = S_{v-drain} / A_v^2$$

Total equivalent input noise voltage

$$e_{nt} = \sqrt{e_n^2 + e_{ni}^2}$$

Input noise voltage (with R input)

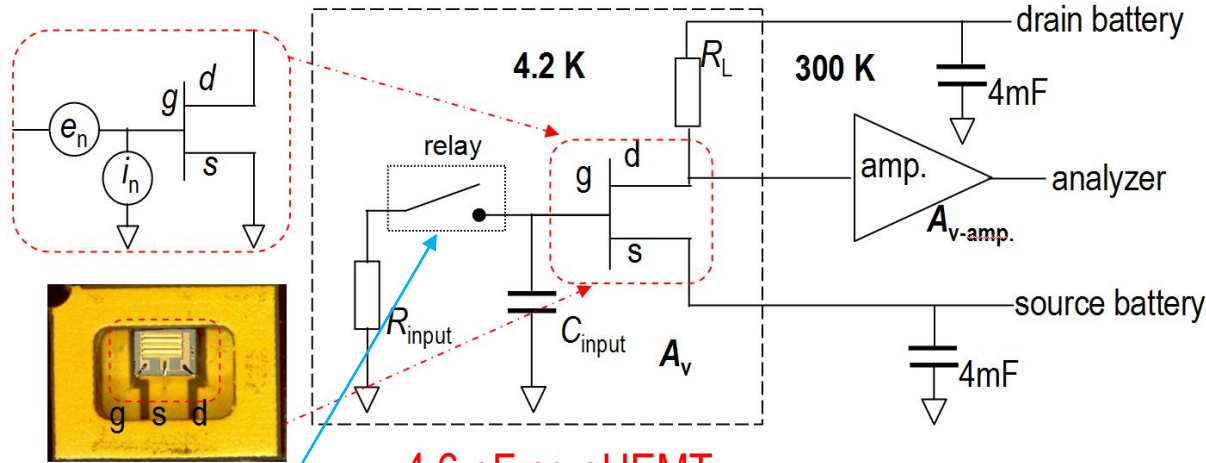
when $e_{ni} \ll e_n$

$$e_n = e_{nt}$$

Input noise current (with R & C input)

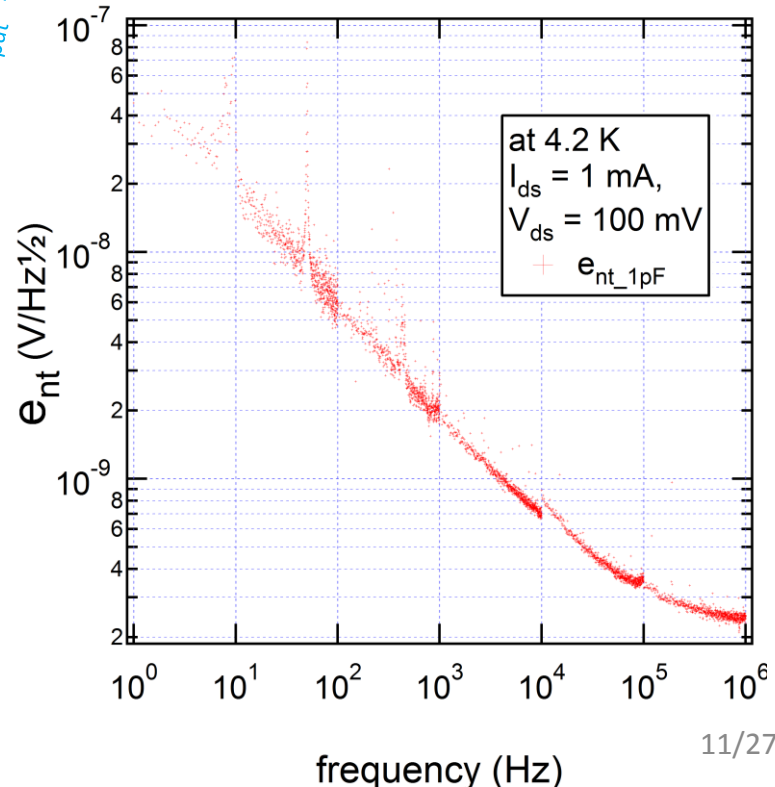
$$i_n = \sqrt{e_{nt}^2 - e_n^2} / |z| = e_{ni} / |z|$$

Appl. Phys. Lett. **105**, 013504 (2014)



4.6 pF cryoHEMT

Total noise voltage measurement setup with $C_{input} = 1\text{pF}$



Characterization: Noise voltage & noise current

Directly measurable parameters:

Channel voltage PSD

$$S_{v-drain} \quad (\text{Power Spectral Density})$$

Voltage gain

$$A_v = \delta V_{out(ds)} / \delta V_{in(gs)}$$

Deduced parameters:

Equivalent input voltage PSD

$$e_{nt}^2 = S_{v-drain} / A_v^2$$

Total equivalent input noise voltage

$$e_{nt} = \sqrt{e_n^2 + e_{ni}^2}$$

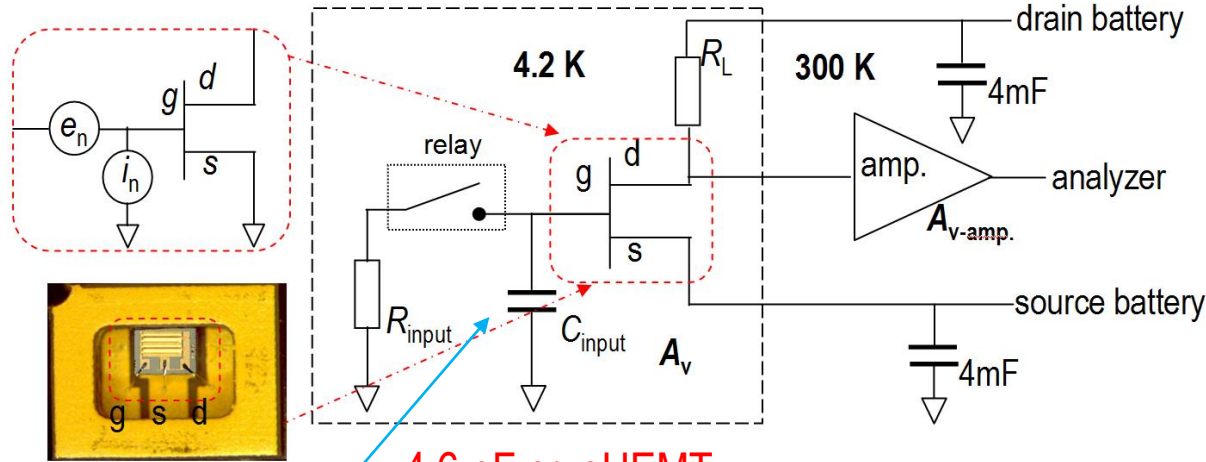
Input noise voltage (with R input)

when $e_{ni} \ll e_n$

$$e_n = e_{nt}$$

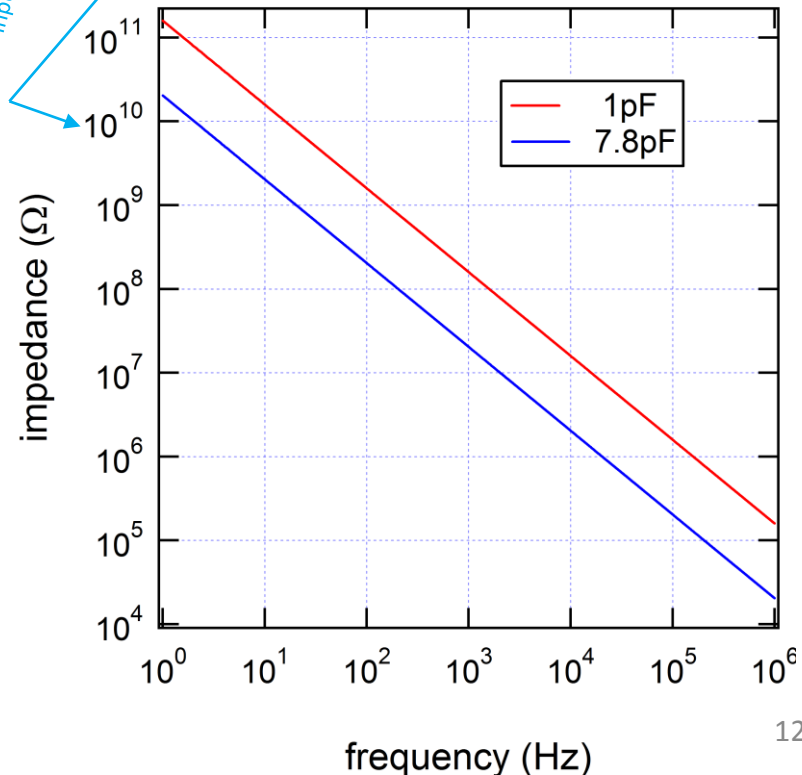
Input noise current (with R & C input)

$$i_n = \sqrt{e_{nt}^2 - e_n^2} / |z| = e_{ni} / |z|$$



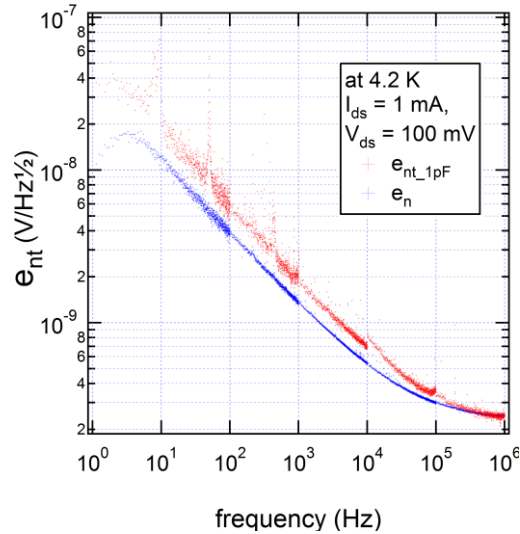
4.6 pF cryoHEMT

Impedances with different C_{input}

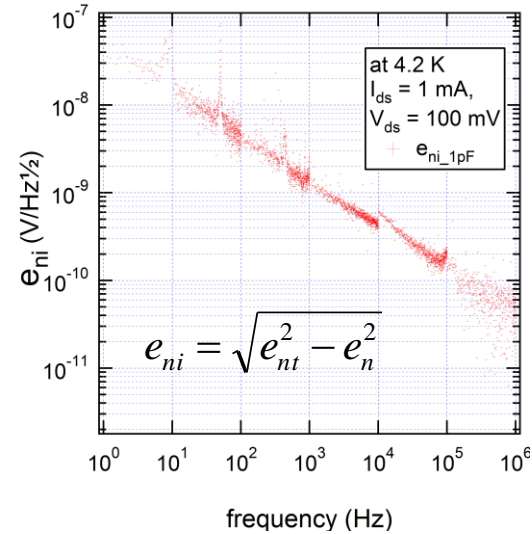


Characterization: noise current measurement

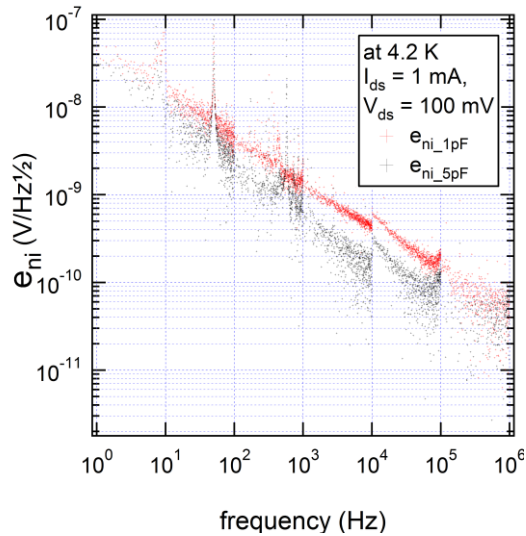
Comparison of capacitor and resistor input



Noise current induced noise voltage



With two different C_{input}

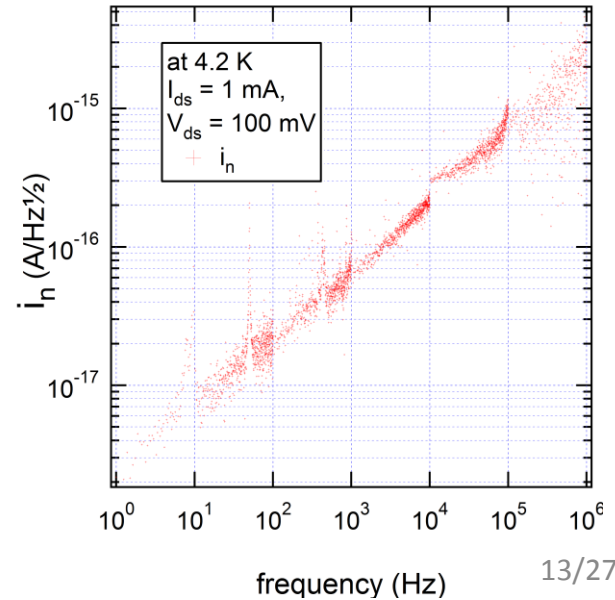


$$e_{ni_1} = i_n \left(\frac{1}{2\pi f (C_{input_1} + C_{HEMT})} \right)$$

$$e_{ni_2} = i_n \left(\frac{1}{2\pi f (C_{input_2} + C_{HEMT})} \right)$$

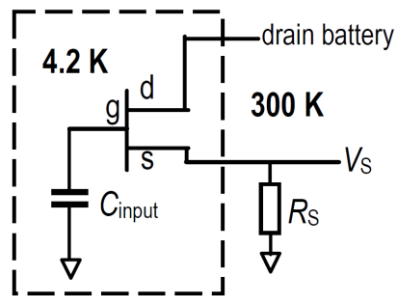
$$C_{HEMT} \approx 6.8 \text{ pF}$$

The deduced noise current



Characterization: gate leakage current measurement

Using a follower configuration, the gate leakage current can be deduced by measuring the variation of the source voltage



For the working point

$$V_{ds} = 100 \text{ mV}, I_{ds} = 1 \text{ mA}$$

$$V_{gs} = -90 \text{ mV}$$

Using C_{input} setup,

$$\text{e.g., } C_{input} = 5 \text{ pF}$$

$$\delta V_{C_{input}} = \delta V_S = 0.5 \text{ mV}$$

$$\delta t = 480 \text{ s}$$

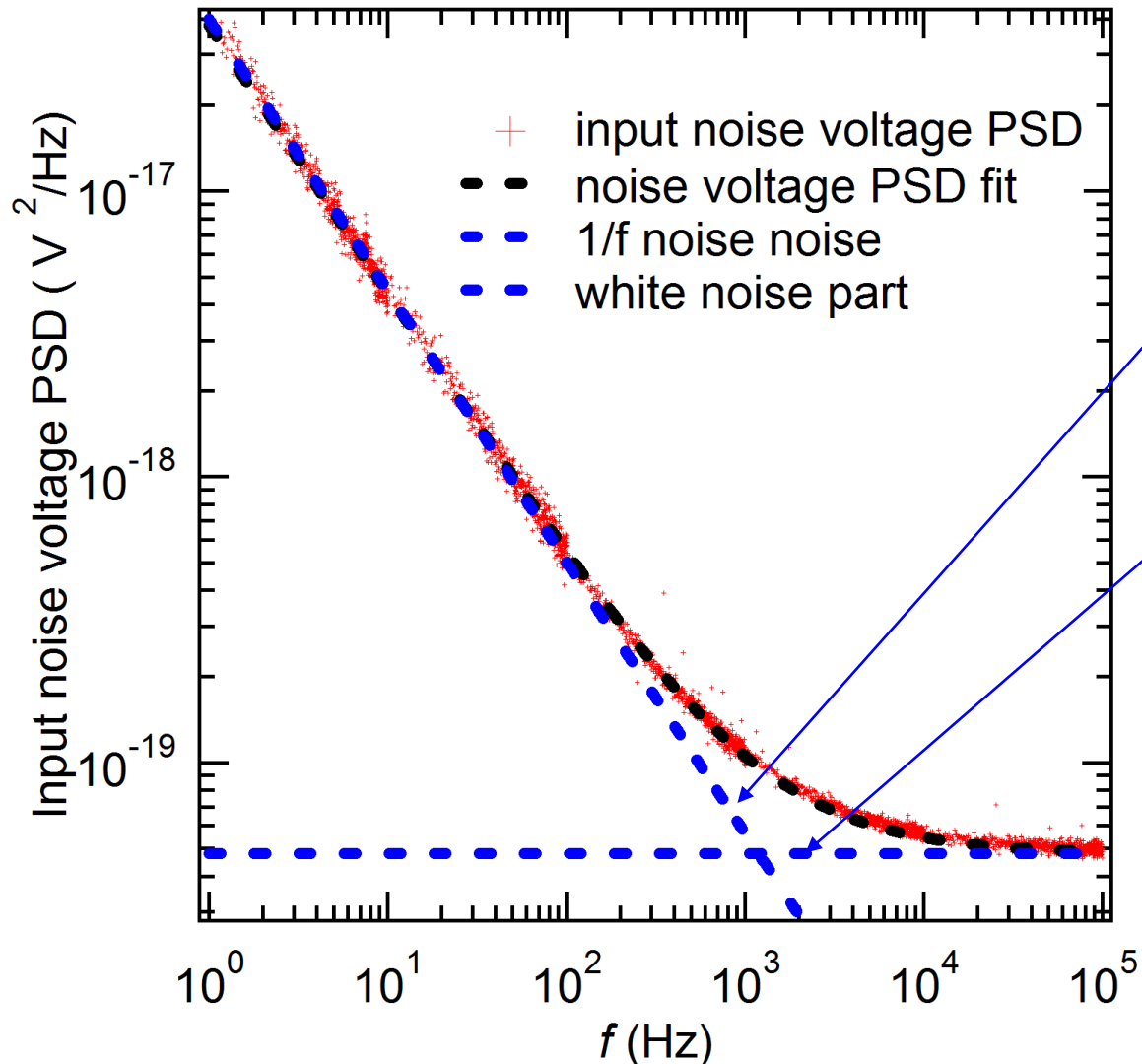
$$I_{gs} = \delta V_{C_{input}} C_{input} / \delta t \approx 5.2 \text{ aA!}$$

$$\text{Input impedance } V_{gs} / I_{gs} \approx 17 \text{ P}\Omega!$$

Appl. Phys. Lett. **105**, 013504 (2014)

Understanding (1/3): noise voltage spectrum compositions

Noise voltage spectrum = 1/f noise + white noise



PSD: Power Spectrum Density

Noise voltage PSD:

1/f noise component:

$$e_{n-1/f}^2 = 4.0 \times 10^{-17} / f^{0.95}$$

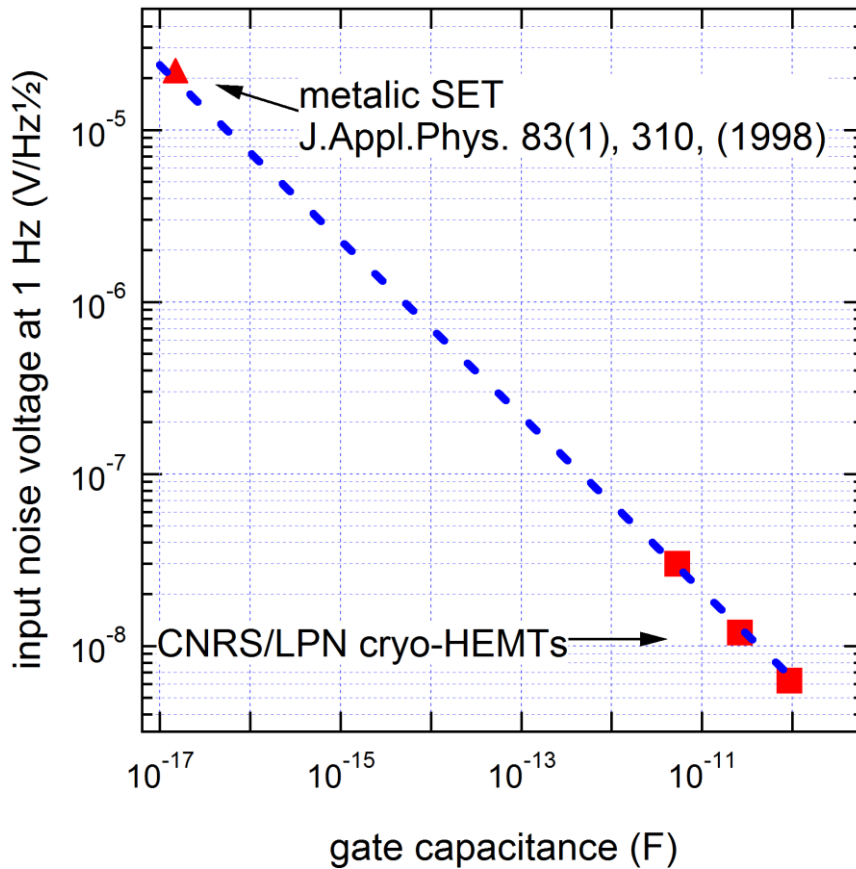
White noise component:

$$e_{n-white}^2 = 4.8 \times 10^{-20}$$

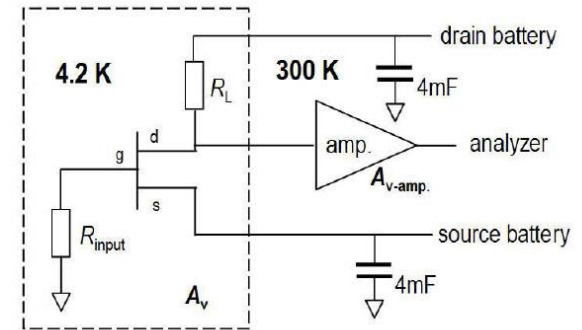
APL 105, 013504 (2014)

Understanding (2/3): input 1/f noise voltage

Input noise voltage e_n vs. gate capacitance C_{gs}



50Ω input: $R_{input} = R_{in} = 50 \Omega$, $R_L = 300 \Omega$



$$e_n \propto \frac{1}{\sqrt{C_{gs}}}$$

$$e_n \propto \frac{1}{\sqrt{C_{gs}}} \sim \frac{1}{\sqrt{N}}$$

fundamental of the 1/f noise voltage in field-effect devices: standard deviation of the average value $\langle N \rangle$ in an open system N (grand canonical ensemble) - central limit theorems

Understanding (3/3): input white noise voltage

Reduced thermal shot noise

$$e_{n-white}^2 \approx \frac{F 2eI_{ds}^2}{g_m^2}$$

F: Fano factor which depends on the gate length

APL 105, 013504 (2014)

Performance: Input noises vs. gate capacitance C_{gs}

Noise voltage e_n , Total noise voltage e_{nt} , Noise current i_n (at 4.2 K)

$L_g \times W$ (μm^2)		1.5×10^5	6.4×10^4	2.0×10^4	2.0×10^3	4.0×10^2
C_{gs} (pF); C_{gd} (pF)		236; 8.9	103; 8.9	33; 3.5	4.6; 1.0	1.8; ~ 0.6
V_{ds} (mV); I_{ds} (mA)		100; 1.0	100; 1.0	100; 1.0	100; 1.0	100; 0.5
g_m (mS); g_d (mS)		52; 0.4	40; 1.2	115; 1.3	44; 1.3	15; 0.8
$f_t = g_m / (2\pi C_{gs})$ (Hz)		3.5×10^7	6.2×10^7	5.5×10^8	1.5×10^9	1.3×10^9
e_n (nV/Hz $^{1/2}$)	@1Hz	5.4	6.3	14	30	100
	@10Hz	1.7	2.1	4.5	12	30
	@100Hz	0.52	0.76	1.5	4.5	10
	@1kHz	0.24	0.34	0.57	1.4	2.7
$e_{n\text{-white}}$ (nV/Hz $^{1/2}$)		0.18	0.22	0.12	0.21	0.4
i_n (aA/Hz $^{1/2}$)	@1Hz	21	15	9.1	2.2	3.6
	@1kHz	6.8×10^2	5.1×10^2	2.4×10^2	70	57
R_n (Ω)	@1Hz	2.6×10^8	4.2×10^8	1.5×10^9	1.4×10^{10}	2.8×10^{10}
	@1kHz	3.5×10^5	6.3×10^5	2.2×10^6	2.0×10^7	3.7×10^7
T_{nt} (mK)	@1Hz	4.1	3.4	4.6	2.4	13
	@1kHz	5.9	6.2	5.0	3.6	5.6

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- **Applications**
- Conclusions and further developments

Applications: Mesoscopic Physics - I

First cryo-preamplifier by F. Pierre, A. Anthore *et al* at C2N (formerly LPN)

In a mK dilution refrigerator, to readout signals at ~ 1 MHz:

Capacitance of the cable from mK to K: 100 pF

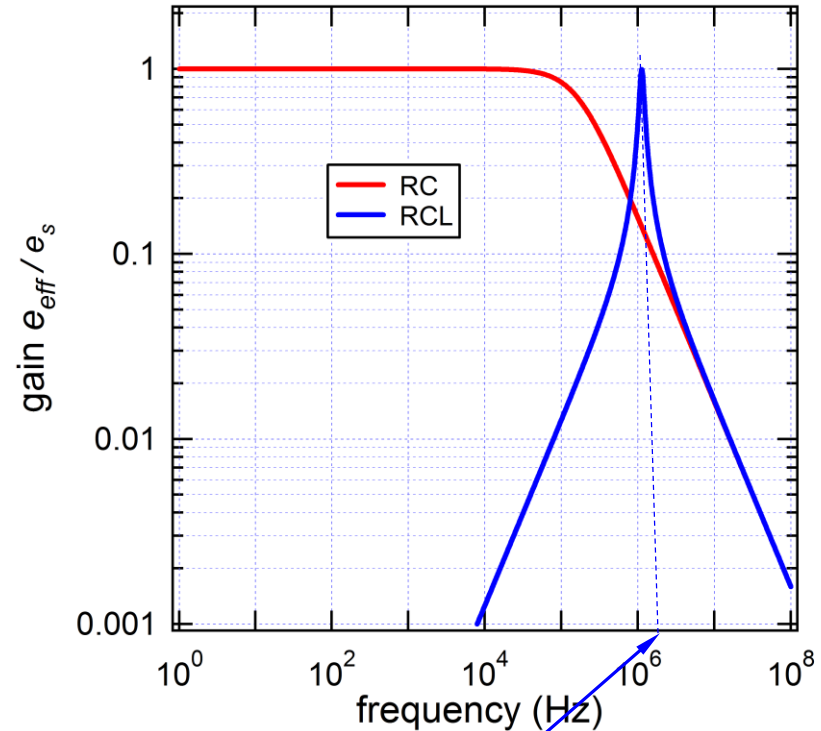
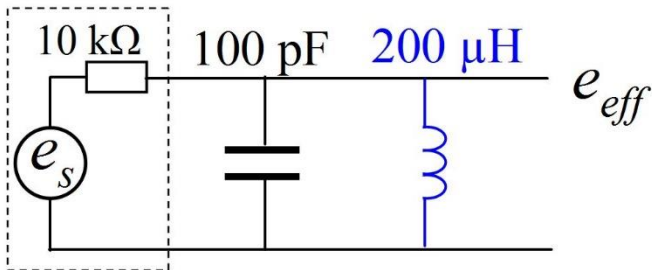
Impedance of to be measured system: 10 k Ω

At 1 MHz, signal gain < 0.2

To avoid signal loss at high f :

Introducing an inductor L for a chosen f

At 1 MHz, signal gain ≈ 1



CryoHEMTs based cryogenic amplifier facilitates:

Quantum limit of heat flow across a single electronic channel *Science* 342, 601 (2013)

Primary thermometry triad at 6mK in mesoscopic circuits *Nature Commun.* 7, 12908 (2016) $\pm 9 \times 10^{-32} \text{ A}^2/\text{Hz}$

Heat Coulomb blockade of one ballistic channel *Nature Phys.* 14, 145 (2018)

$$f_0 = \frac{1}{2\pi\sqrt{LC}}$$

Applications: Mesoscopic Physics - II

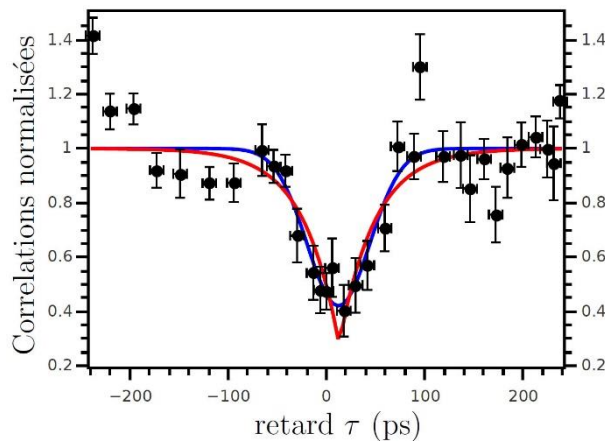
Based on the work by F. Pierre, A. Anthore *et al* @ LPN

G. Fève *et al* at LPA, ENS Paris

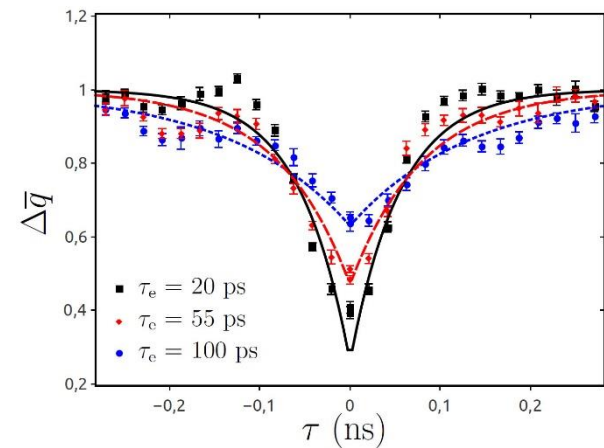
Comparisons: NF LI-75A and cryoHEMT (from V. Freulon thesis at LPA, ENS Paris)

$$\text{Signal-to-noise ratio } SNR: SNR = \frac{\int_{f_{min}}^{f_{max}} du S_v^p(u)}{\left[\int_{f_{min}}^{f_{max}} du (S_v^a)^2 / 2 \right]^{1/2}} \sqrt{T_{meas}}$$

PSD of the measured voltage: S_v^p ; PSD of the amp input noise voltage e_n : $S_v^a = e_n^2$ and measurement duration T_{meas} \rightarrow For a fixed SNR: $T_{meas} \sim e_n^4$



By NF LI-75A at 300 K,
for one point: $2.56 \times 10^4 \text{s} \approx 7 \text{ hours!}$
 $SNR = 10!$



By cryoHEMT preamplifier at $\leq 4.2 \text{ K}$,
for one point: $2.25 \times 10^2 \text{s} \approx 4 \text{ minutes!}$
 $SNR = 30!$

Hong-Ou-Mandel experiment for temporal investigation of single-electron fractionalization,
Nature Commun. 6, 20 (2015)

Comparisons: NF LI-75A at 300 K and cryoHEMT amplifier at 4.2 K

	According to NF Corporation	4.6 pF cryoHEMT Made at CNRS/LPN
Operating temperature	300 K	0 K to 77 K
	NF LI-75A Data obtained @ 300 K	CryoHEMT amplifier Data obtained @ 4.2 K Power consumption: 0.25mW
Input impedance	100 MΩ // 50 pF Voltage gain of 100	10 PΩ* // 15 pF Voltage gain of about 10
Noise voltages	2 nV/Hz ^{1/2} at 1 kH	1.42 nV/Hz ^{1/2} at 1 kHz 0.3 nV/Hz ^{1/2} at 100 kHz 0.24 nV/Hz ^{1/2} at 1 MHz
Noise currents	<i>14 fA/Hz^{1/2} *</i>	60 aA/Hz ^{1/2} at 1 kHz 0.7 fA/Hz ^{1/2} at 100 kHz 2 fA/Hz ^{1/2} at 1 MHz

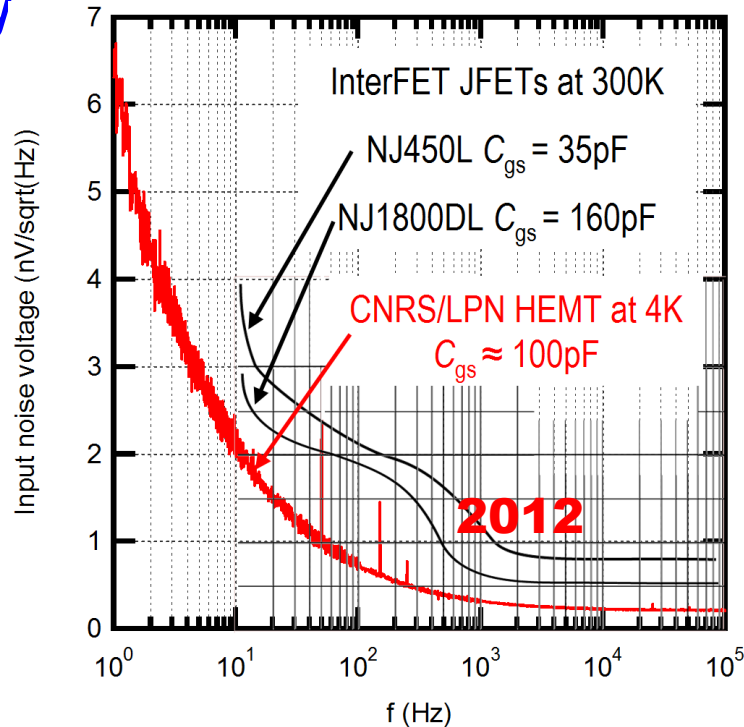
**Eur. Phys. J. Special Topics 172, 163 (2009)*

***cryoHEMT input impedance > 10 P Ω : 10¹⁶ Ω**

Applications: Astrophysics CDMS

B. Sadoulet team at UC Berkeley

- Comparison of the input noise voltage between cryoHEMT and JFETs (by the C2N)



- Comparison of the heat dissipation and the sensibility threshold

	Temperature	Heat dissipation	Sensibility threshold
JFET	150 K	5.5 mW	133 electrons
CryoHEMT	4.2 K	0.1 mW	35 electrons

An HEMT-Based Cryogenic Charge Amplifier for Sub-kelvin Semiconductor Radiation Detectors, *J. Low Temp. Phys.* 184, 505 (2016)

A HEMT-Based Cryogenic Charge Amplifier with sub-100 eVee Ionization Resolution for Massive Semiconductor Dark Matter Detectors

<http://arxiv.org/abs/1611.09712> (2018)

Applications of cryoHEMTs and Publications in

- **Mesoscopic Physics:** C2N, Palaiseau; LPA ENS Paris; IN, Grenoble

1 *Science*; 1 *Nature Physics*; 2 *Nature Commu.*

- **Low Temperature STM:** LPS, Orsay; Leiden Univ.

Charge trapping and super-Poissonian noise centers in a cuprate superconductor

Nature Physics (accepted) (2018)

Atomic scale shot-noise using cryogenic MHz circuitry

Review of Scientific Instruments (accepted) (2018)

- **Low Temperature Nano-mechanical Resonators:** ICFO, Barcelona

Ultrasensitive displacement noise measurement of carbon nanotube mechanical resonators

Applied Physics Letters 113, 063104 (2018)

Improving the read-out of the resonance frequency of nanotube mechanical resonators

Nano Letters 18, 5324 (2018)

- **Low Temperature Detectors:** IRFU, CEA-Saclay

Toward large μ -calorimeters x-ray matrices based on metal-insulator sensors and HEMTs/SiGe cryo-electronics

Proc. SPIE 2016, vol.9905, 99050S (2016) (*for X-ray detection*)

High impedance TES with classical (cryogenic HEMTs) readout electronics: a new scheme toward large x-ray matrices

Proc. SPIE 10699, *Space Telescopes and Instrumentation 2018: Ultraviolet to Gamma Ray*, 106995T (2018)

- **Superconductor Circuits:** LPS, Orsay; Collège-de-France, Paris

- **Cryogenic Dark Matter Detection:** Edelweiss III: IPNL, Lyon; Super-CDMS: SLAC-Stanford,

Berkeley; Tsinghua Univ. Beijing

- **CryoHEMTs Based Amplifiers by « Stahl Electronics »**

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Conclusions

High impedance and low frequency cryoelectronics

	Low Frequency		High Frequency
	Low Impedance	High Impedance	Low Impedance
Room Temperature	JFETs BJTs	JFETs	HEMTs
Low Temperature ($T < 100$ K)	HEMTs $f \geq$ MHz CryoHEMTs	CryoHEMTs	HEMTs $f > 1$ GHz CryoHEMTs Tested up to 150MHz

Commercially available devices

Commercially available devices

Made at CNRS/C2N
Formerly: CNRS/LPN

Our cryoHEMTs facilitate the following accomplishments:

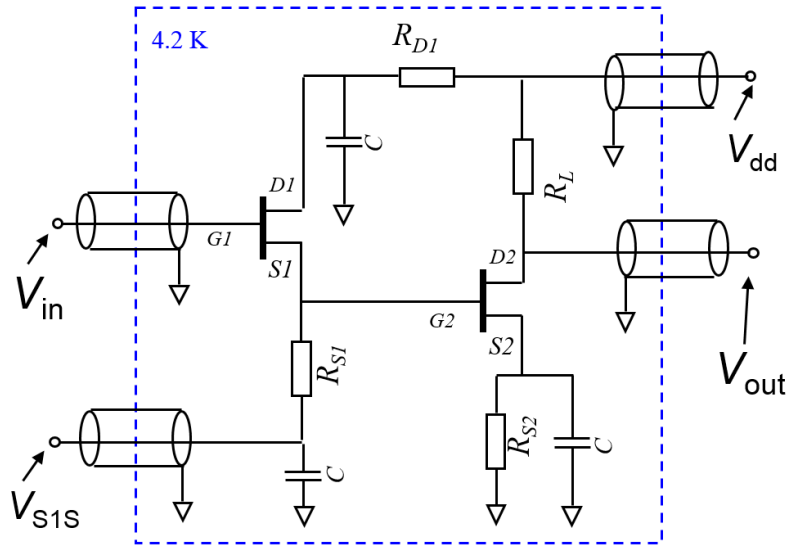
- Reaching unprecedented low noise current and decrease significantly noise voltage
- Attaining unrivaled readout rates and improve the *Signal-to-Noise Ratio*
- Realizing novel experimental observations

Their implementation has already resulted in the publications of

1 Science, 2 Nature Phys., 2 Nature commu. 1 Nano Lett.

Further Developments: LT and LF amplifier

- Follower + Amplifier: low input capacitance and low noise voltage at LF



$$g_{m1}R_S > 100 \rightarrow C_{in} \approx C_{gd1} \text{ instead of } C_{gs1}$$

Benefits of the follower:

- enabling cryoHEMTs with very large C_{gs} (to reduce LF noise)
- minimizing feedback effect
- having low output impedance $1/g_{m1}$

Disadvantage of “follower + amplifier”:

- minimum input noise voltage e_1 increases to $\sqrt{e_1^2 + e_2^2}$

Using two $C_{gs} = 236\text{pF}$ cryoHEMTs:

$C_{input} = 10\text{pF}$ and $R_{input} > 10^{15}\Omega$

$e_n = 1\text{nV}/\text{Hz} @ 60\text{Hz}$

